

# The ZL2BMI DSB TRANSCEIVER.

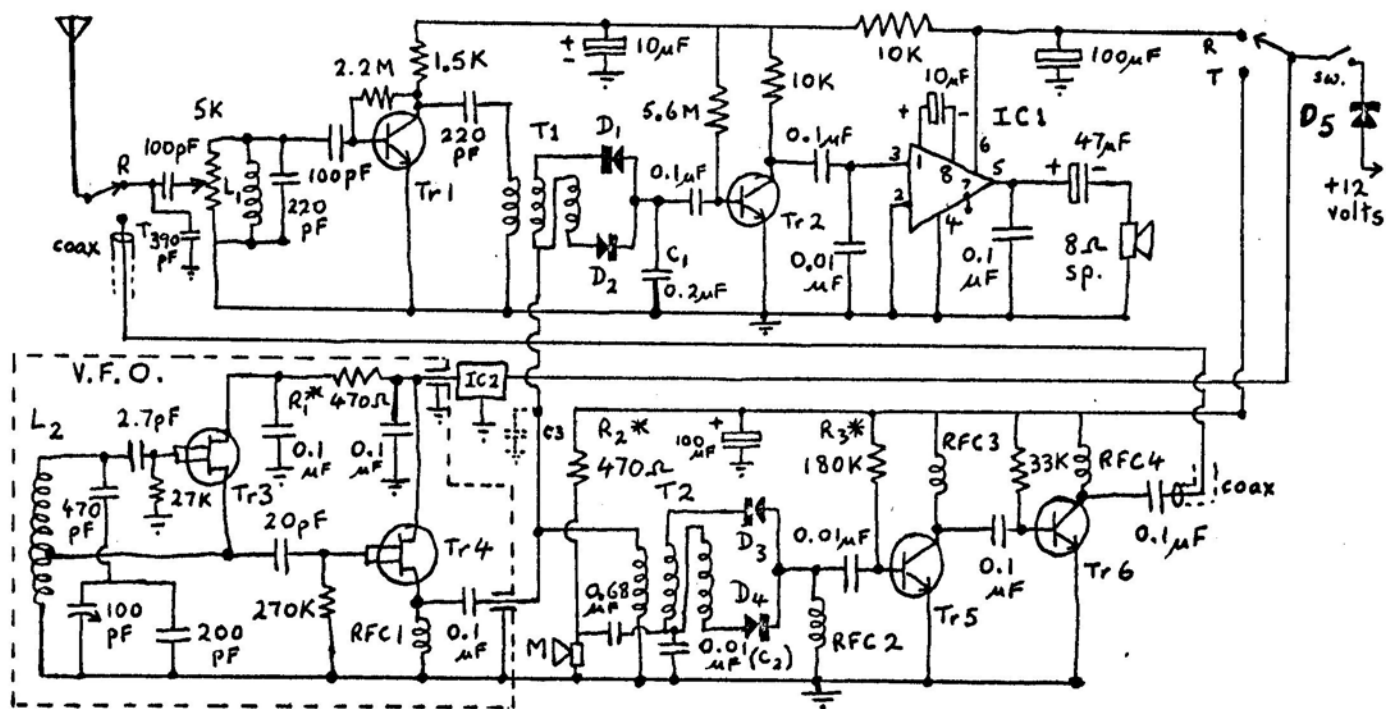


Fig 1.

## Components : — 18

$L_1$  - 45 turns on small iron dust toroid. (A T50/2 with 40 turns may be better)

$L_2$  - 50 turns, tapped at 8 turns, on 5mm slug-tuned former.

$T_1/T_2$  - 7 trifilar windings, approx 35 swgenam. wire on 6mm bead 2.5mm hole,

$RFC_1/RFC_2/RFC_3$  - 10 turns thru' ferrite bead (approx  $150\mu H$ ) (Neosid F7 ferrite)

$RFC_3$  -  $2\frac{1}{2}$  turns thru' 6-hole bead (approx  $15\mu H$ ). M - Carbon mike insert.

$D_1-D_4$  - BAT 81 (H.C.D's)  $D_5$  - 1N4001 (reverse polarity protection)

$Tr_1, Tr_2, Tr_5$  - BC338.  $Tr_3, Tr_4$  - BF960 dual gate FET.  $Tr_6$  - BD139.

IC1 - LM386N/3. IC2 - 78L08 (8V, 100mA regulator)

## NOTES

### V.F.O.

The reason for using UHF dual-gate FETs is simply that they were available cheaply. Other dual-gate FETs should work; J-FETs would also probably work but may require changing the value of the 2.7pF capacitor or the tapping point on the coil.

$R_1$  was originally specified as  $100\Omega$  but was altered to  $470\Omega$  or even  $820\Omega$  (in one case) to reduce the current drain of the oscillator.

Effectively,  $Tr_3$  operates on about 2-3 volts. The capacitor on the drain of  $Tr_3$  may be a lower value than  $0.1\mu F$  in some cases.

The value of the coupling capacitor to the buffer, may also vary.

Capacitor  $C_3$ , from the output of the V.F.O. to ground, may be included to reduce the VFO drive to the correct level.  $C_3$  would be a value up to about  $2000pF$ . It may also have in parallel with it, a resistor of  $15-50\Omega$ .

The feedthru' for VFO power is  $1000pF$  type. The output feedthru' is  $0pF$ .

## Receive Board

The front end tuned circuit is very simple and not particularly selective. A  $50\Omega$  aerial, especially a dipole or balanced type, will not usually cause trouble with B.C. breakthrough. Some spurious signals from 40m and higher may be heard, but these are not usually troublesome at the time when 80m is best for QRP work.

There is plenty of space to experiment with a better front-end if you wish. Alternatively, a simple pi-net filter at the aerial socket would benefit both receive and transmit. (See fig. 2).

Note that the VFO port of  $T_1$  requires a d.c. path to earth, which is normally provided through a winding of  $T_2$ . If  $T_2$  is disconnected, it would be necessary to add a small R.F.C. to replace it, in order for the receive mixer to work

$C_1$  may be raised in value to reduce the audio 'highs'. The lower tone may be more pleasant, but will also reduce sensitivity slightly.

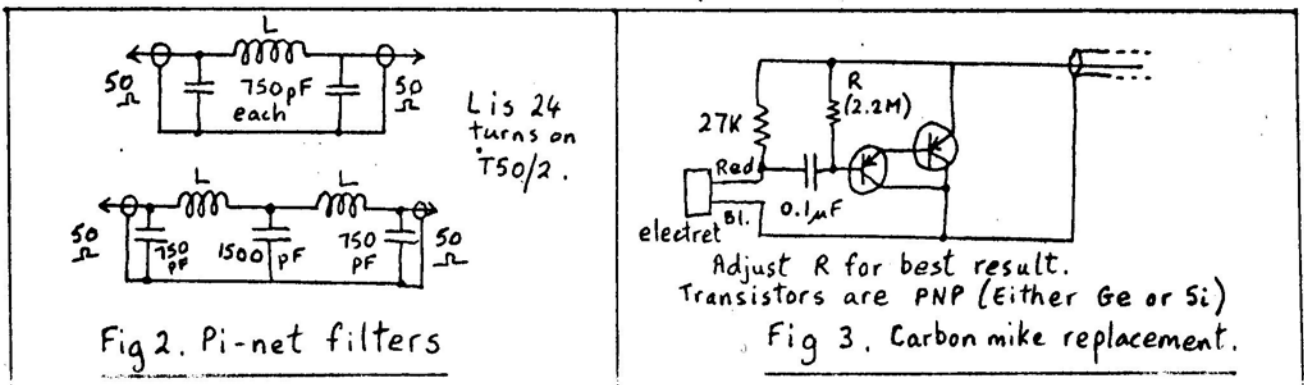
## Microphone, Balanced Modulator and R.F. Amplifier

While the carbon mike is simple, it is quite effective.  $R_2$  may vary in value, depending on the particular mike. If you wish to experiment, there is a circuit (fig. 3), which I have used as a direct replacement (all components in the mike case), for a carbon mike. It still needs some refinement, and it is possible that  $R_2$  should be raised to about 10K with a circuit such as this. The  $0.68\mu\text{F}$  capacitor feeding the bal. mod. may also be altered to increase or decrease the modulation. Note that  $D_1$ - $D_4$  could be replaced by 1N914s, (matched pairs), but the carrier null may not be quite so good.

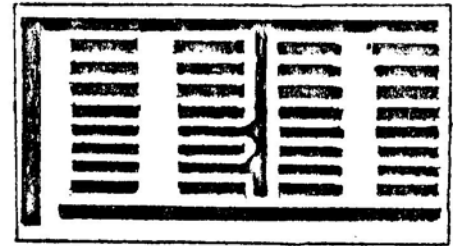
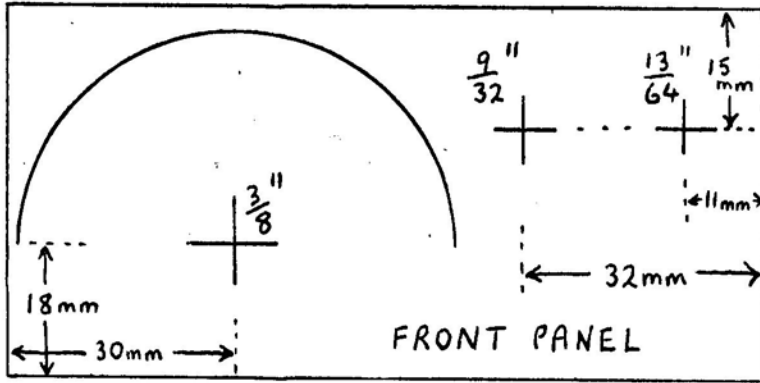
$R_3$ , the bias resistor for  $Tr_5$ , can be reduced to 100K. This will give up to 50% extra output; however  $Tr_5$  will run quite hot in this case (though generally they will stand this O.K.)

When run on 14-15 volts, the transmitter will put out significantly more power than on 12 volts, possibly up to about 3 watts.

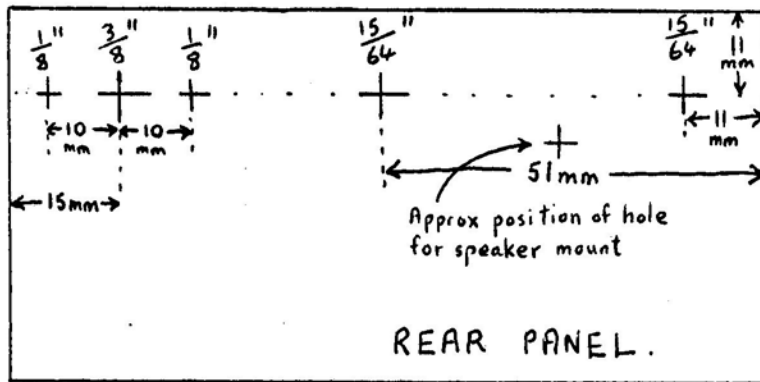
Raising the output power with another amplifier is not advisable unless a good deal more filtering is provided.





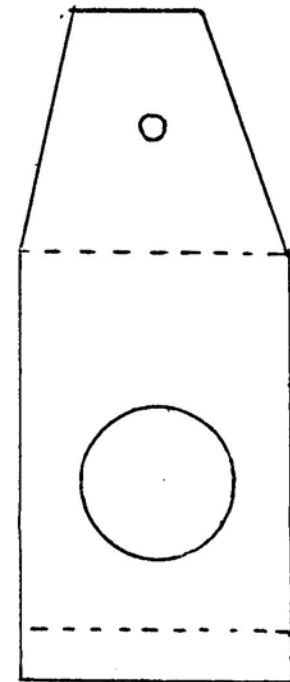


Receive Board.



r.f. amp board.

Drilling Layouts (to scale)



Speaker bracket  
(Vinyl floor covering)  
material

